PROPOSED STACKED TOWNHOUSE DEVELOPMENT 6633 MCLEOD ROAD, NIAGARA FALLS

FUNCTIONAL SERVICING DESIGN BRIEF NEW STORM, SANITARY AND WATER SERVICES

REV 0 - August 17, 2022

PREPARED BY:



HALLEX PROJECT #220326

HALLEX NIAGARA 4999 VICTORIA AVENUE NIAGARA FALLS, ON L2E 4C9 HALLEX HAMILTON 745 SOUTH SERVICE ROAD, UNIT 205 STONEY CREEK, ON L8E 5Z2

Hallex Project #220326 August 17, 2022 Rev #0

TABLE OF CONTENTS

I INT	TRODUCTION	1
	(ISTING MUNICIPAL INFRASTRUCTURE	1
2.1	EXISTING SITE DRAINAGE	1
	CTOPA CELUED	2
2.2	STORM SEWERSANITARY SEWER	2
2.3	SANITARY SEWER	2
2.4	WATERMAIN	2
	TORM SEWER/DRAINAGE SYSTEM	2
3.1	PRE-DEVELOPMENT SITE FLOW	2
3.2	POST-DEVELOPMENT SITE FLOW	2
3.3	STORMWATER QUANTITY CONTROL	3
	STORMWATER QUALITY CONTROL	3
3.4	STORMWATER QUALITY CONTROL	
4 CA	ANITARY SEWER SYSTEM	4
		5
5. W	ATER DISTRIBUTION SYSTEM	6
6. CC	ONCLUSION	,

PRE-DEVELOPMENT CATCHMENT AREA PLAN

POST-DEVELOPMENT CATCHMENT AREA PLAN

EXHIBITS - Storm, Sanitary and Water Services Design

1. INTRODUCTION

The proposed 18-unit stacked townhouse development consists of the demolition of the existing 1-storey residential dwelling and detached garage complete with asphalt parking areas. The proposed development consists of the construction of a 3-storey building, asphalt laneway, asphalt parking areas and grass areas. The subject development is located at 6633 McLeod Road, which is East of the Dorchester Road and McLeod Road intersection in the City of Niagara Falls, ON.

The purpose of the service assessment is to determine the functional sizing of the proposed storm, sanitary and water services in addition to the post-development flows from the site to determine the impact on the existing municipal infrastructure.

2. EXISTING MUNICIPAL INFRASTRUCTURE

2.1 EXISTING SITE DRAINAGE

The existing site currently drains from the North side to the South side of the property via overland flow as shown in **Figure 1** – NPCA Watershed Map – Existing Site Contours. The overland flow drains to the existing sewer at McLeod Road.

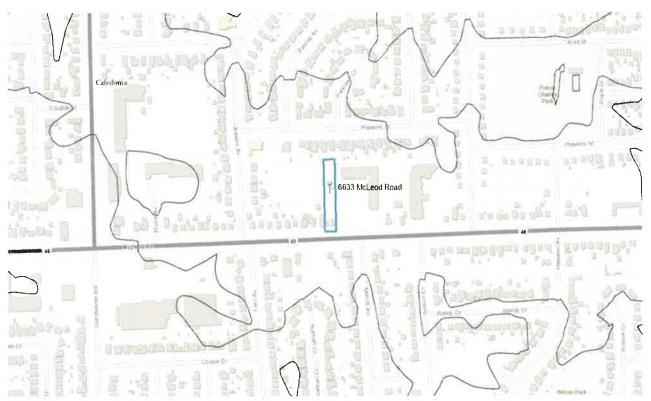


Figure 1 - NPCA Watershed Map - Existing Site Contours

2.2 STORM SEWER

The existing site is currently not serviced with a storm connection, the subject site drains via overland flow to McLeod Road. The existing storm infrastructure within McLeod Road consists of a 1200mm municipal storm sewer which drains Westerly towards Dorchester Road.

2.3 SANITARY SEWER

The existing site is currently serviced with a sanitary lateral connection; however, the size and location of the existing sanitary lateral is unknown. The existing sanitary infrastructure at McLeod Road consists of a 525mm municipal sanitary sewer and a 600mm combined sewer which drains Westerly towards Dorchester Road.

2.4 WATERMAIN

The existing site is currently serviced with a water service connection to McLeod Road; however, the size and location of the existing water service is unknown. The existing watermain infrastructure at McLeod Road consists of a 300mm municipal watermain.

3. STORM SEWER/DRAINAGE SYSTEM

3.1 PRE-DEVELOPMENT SITE FLOW

The total drainage area for the subject development is 0.225 hectares with an existing runoff coefficient of 0.32 based on the existing roof, asphalt and grass surfaces. The catchment area plan for the pre-development site condition is provided on Hallex Sketch CSK1, attached.

Utilizing the rationale method (Q = CiA/360) and the minimum recommended time of concentration of 10 minutes, the allowable peak flow for the pre-development site is as follows:

Storm Event Storm Flow
5-year Storm 16.9 L/s

These flows are calculated using the City of Niagara Falls intensity-duration-frequency curves. The predevelopment flows for the proposed development are provided in Exhibit #1 for the five -year storm at the end of the design brief, attached.

3.2 POST-DEVELOPMENT SITE FLOW

The proposed development includes the 18-unit building, asphalt laneway and parking areas and grass areas. The grading for the site will ensure drainage through the proposed storm sewer for storm water quantity and quality controls. The total drainage for the site consists of 0.225 hectares with a calculated runoff coefficient of 0.72 based on the proposed roof, asphalt and grass surfaces.

Proposed Stacked Townhouse Development 6633 McLeod Road, Niagara Falls Issued for Approval Hallex Project #220326 August 17, 2022 Rev #0

The proposed storm sewer for the site will then discharge to the existing 1200mm municipal storm sewer at McLeod Road. The catchment area plan for the post-development site condition is provided on Hallex Sketch CSK2, attached.

Utilizing the rationale method (Q = CiA/360) and the minimum recommended time of concentration of 10 minutes, the calculated peak flow for the post-development site is as follows:

Post-Development

Storm Event

Storm Flow

5-year Storm

37.8 L/s

These flows are calculated using the City of Niagara Falls intensity-duration-frequency curves. The post-development flows for the proposed development are provided in Exhibit #2 for the five -year storm at the end of the design brief, attached.

3.3 STORMWATER QUANTITY CONTROL

The post-development storm water runoff for the subject site will increase by 20.9 L/s for the five-year storm. As such, storm water detention will be required for the proposed development.

Stormwater quantity controls for the site can be achieved by utilizing an orifice plate within a manhole prior to discharging to the existing 1200mm municipal storm sewer at McLeod Road.

The orifice plate will ensure the post development runoff is controlled to the pre-development runoff rate for the five-year storm event. The resulting 36 m³ volume generated for the five-year storm event, can be stored within a proposed underground storage chamber system or a storm sewer system consisting of oversized storm sewers, catch basins / manholes prior to discharging to the existing 1200mm municipal storm sewer at McLeod Road.

3.4 STORMWATER QUALITY CONTROL

Stormwater quality controls for the site can be achieved by utilizing a Hydrostorm HS4 prior to draining to the existing 1200mm municipal storm sewer at McLeod Road. This will achieve a total suspended solids removal of at least 88% based on the above post-development site conditions. This value is greater than the required 'Normal' treatment of 70% as indicated in the MOE Stormwater Management Planning and Design Manual, dated March 2003 (refer to Chapter 3: Environmental Design Criteria, Section 3.3.1.1. Level of Protection).

4. SANITARY SEWER SYSTEM

Given the site is to be completely redeveloped for the proposed 18-unit stacked townhouse development, all existing sanitary laterals are to be located, capped and abandoned as required at the municipal sanitary sewer. A new sanitary lateral shall be proposed to connect to the existing 525mm diameter municipal sanitary sewer at McLeod Road.

The building development is currently in the concept phase; therefore, the following assumptions based on the architectural drawings are made in carrying out the calculations:

- The 18-unit stacked townhouse development consists of 12 one-bedroom townhouse units and 6 two-bedroom townhouse units. Each townhouse is assumed to have a maximum of 2 persons per bedroom.
- The existing fixtures and the number of existing plumbing fixtures indicated in Exhibit #3 were provided by the owner and must be field verified prior to construction.
- The plumbing fixtures and the number of plumbing fixtures indicated in Exhibit #4 are assumed and may not represent the final building plumbing design.

The peak pre-development drainage rate for the existing residential dwelling is determined to be 95.6 L/min based on the existing fixtures and fixture units shown in Exhibit #3 attached. Table 7.4.10.5 in the Ontario Building Code is used to determine probable peak drainage rates for the total fixture units. The wastewater generation for the existing residential dwelling is determined to be 1600 L/day using Table 8.2.1.3A of the Ontario Building Code as shown in Exhibit #3, attached.

The peak post-development drainage rate for the proposed 18-unit stacked townhouse development is determined to be 325.9 L/min based on the fixtures and fixture units shown in Exhibit #4 attached. Table 7.4.10.5 in the Ontario Building Code is used to determine probable peak drainage rates for the total fixture units. The wastewater generation for the proposed 18-unit stacked townhouse development is determined to be 13200 L/day using Table 8.2.1.3A of the Ontario Building Code as shown in Exhibit #4, attached.

Based on the above, Hallex recommends a minimum 200mm diameter sanitary sewer @ 1.0% in order to service the townhouse block complete with a minimum 100 diameter sanitary lateral @ 2.0% to service each stack of townhouse units. The proposed 200mm diameter sanitary sewer shall convey flows from the subject site to the existing 525mm diameter municipal sanitary sewer at McLeod Road.

5. WATER DISTRIBUTION SYSTEM

Given the site is to be completely redeveloped for the proposed 18-unit stacked townhouse development, all existing water services are to be located, capped and abandoned as required at the municipal watermain. A new water service shall be proposed to connect to the existing 300mm diameter municipal watermain at McLeod Road.

The building development is currently in the concept phase; therefore, the following assumptions based on the architectural drawings are made in carrying out the calculations:

- The 18-unit stacked townhouse development consists of 12 one-bedroom townhouse units and 6 two-bedroom townhouse units.
- The existing fixtures and the number of existing plumbing fixtures indicated in Exhibit #5 were provided by the owner and must be field verified prior to construction.
- The plumbing fixtures and the number of plumbing fixtures indicated in Exhibit #6 are assumed and may not represent the final building plumbing design.
- The Townhouse block is assumed to be of wood-frame construction and will not have sprinklers installed throughout the building.

The pre-development domestic water demand for the existing residential dwelling is determined to be 80.3 L/min based on the existing fixtures and fixture units shown in Exhibit #5 attached. Table 7.4.10.5 in the Ontario Building Code is used to determine water demands for the total fixture units.

The post-development domestic water demand for the proposed development is determined to be 292.7 L/min based on the fixtures and fixture units shown in Exhibit #6 attached. Table 7.4.10.5 in the Ontario Building Code is used to determine water demands for the total fixture units.

Using the calculations provided in the Fire Underwriters Survey – 1999 Water Supply for Public Fire Protection, the minimum water supply flow rate for fire protection is determined to be 10000 L/min for the building based on the above assumptions as shown in Exhibit #7, attached. There is one existing municipal fire hydrants located near the site. The hydrant is located approximately 20 meters from the Southwest corner of the site on the South side of McLeod Road.

Based on the above, Hallex recommends a minimum 50mm diameter water service to be installed to provide water supply from the proposed townhouse block to the existing 300mm diameter municipal watermain at McLeod Road.

6. CONCLUSION

The aforementioned calculations and recommendations for the storm, sanitary and water services are based on the current design for the site as of writing this report. A final sealed report, complete with updates to the recommendations made in this report, may be required based on the final site design.

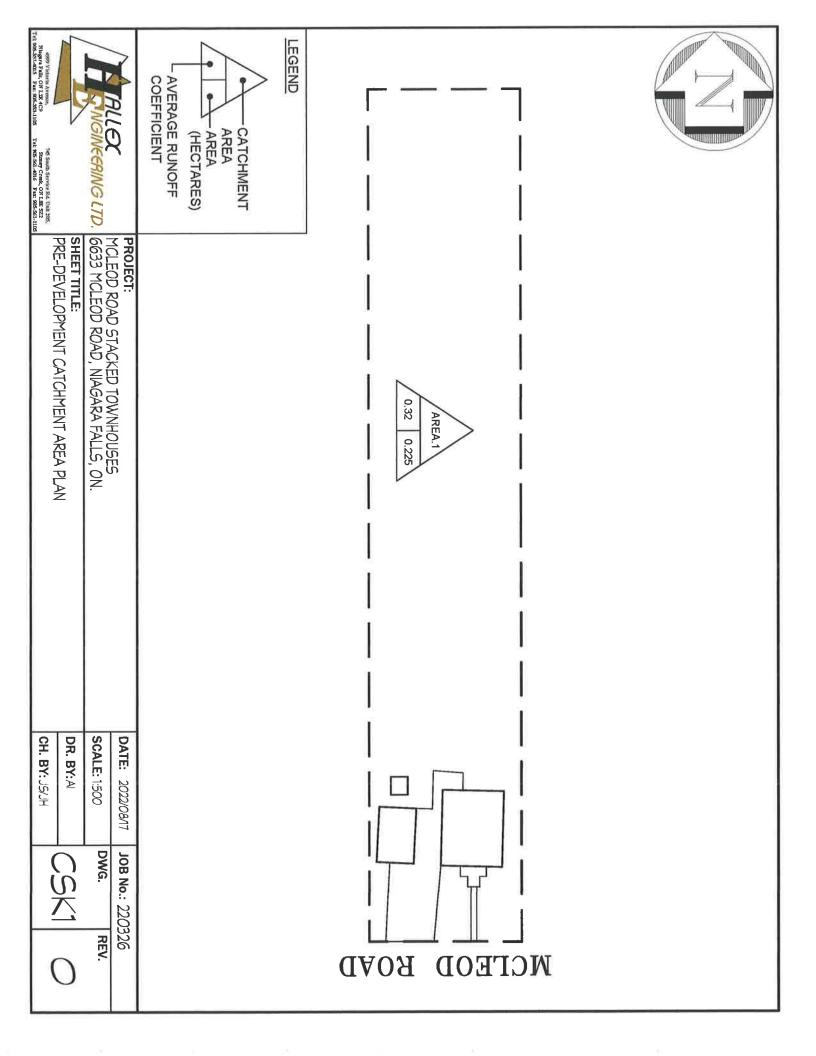
We trust this report meets your approval. Please contact the undersigned should you have any questions or comments.

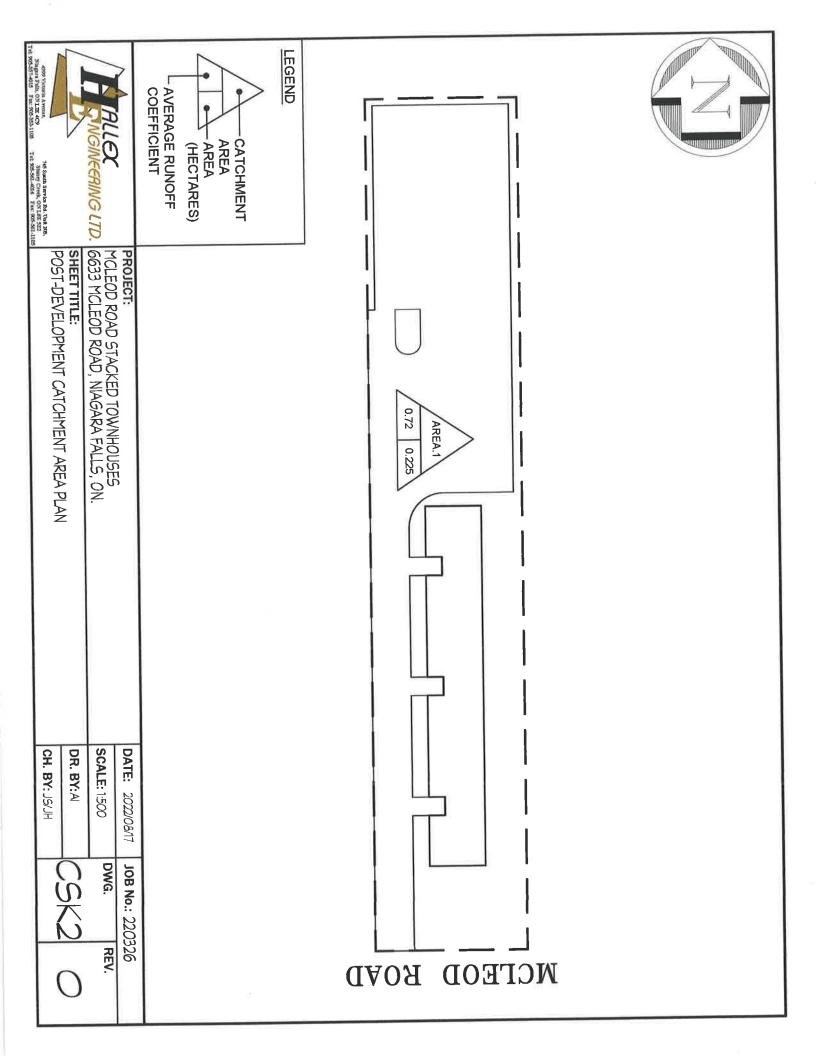
Yours truly,
HALLEX ENGINEERING LTD



Jim Halucha P.Eng Civil/Structural Engineer Anthony Infurna, C.Tech, rcji

Civil Designer/Project Coordinator







6633 McLeod Road - Stacked Townhouses Exhibit #1 - 5 Year Pre - Development Calculations

2022-08-16 Job: 220326

MUNICIPALITY: Niagara Falls

manning's n = 0.013 Conc Pipe 0.013 PVC Pipe 0.024 Corr. Stl Pipe

Rainfall Intensity Values =

A= 719.500 B= 6.340 C= 0.769

	1013.3	5041.4	Ē	ě.	æ	t	0.201	(30)	٠	•	Grass
	217.8	18149.2	(A		a	9	0.012	а			Paved
	229.9	19157.5	ŧ	ì		x	0.012	n	•	1	Roof
0.0169	1461.0	60497	84	N/A	10.00	0.225 0.225	0.225	N/A	Street	Area.1	1
(m³/s)	(m³/d)	m³/ha*day	mm/hr	(min)	(min)	(ha)	(ha)	(m)	NOG G	Noge	
Flow	Flow	Intensity of Runoff	Intensity	Sectio	ment Total Upper Section	Total	ment Total	of Pipe	Ž 7	From	Pipe
Flows	Design	Unit rate	Rainfall	Time	Flow	e a	Area	Length		Location	

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Velocity Range:

	Gravel Surface	Paved Surface	Roof Structure	
	C "	C II	C II	
,	0.60	0.90	0.95	
		Maximum Velocity =	Minimum Velocity =	
		6.00 m/s	0.80 m/s	

Time of Concentration =

Perm. Paver Grass Surface

000

0.60 0.30 0.25

10 min



Exhibit #2 - 5 Year Post - Development Calculations 6633 McLeod Road - Stacked Townhouses

2022-08-16 Job: 220326

Rainfall Intensity Values = C B } 719.500 6.340 0.769

manning's n =

0.013 PVC Pipe 0.013 Conc Pipe 0.024 Corr. Stl Pipe 0.035 Grass Swale

Upper (min) 10.00	(min)	mm/hr	84 42348 - 19157.5 - 18149.2 - 5041.4	(m ^{-/d}) 3264.8 632.2 2304.9	(m³/s) 0.0378		N/A	z	' ' A	IA NIA	IA NIA NIA	IA NIA NIA NIA
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Cum To	, 5	ntensity	of Runoff	Cum Flow	1 (_	Control	_	Control Slope	Control Slope	Control Slope Capacity Control	Control Slope Capacity Control
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Flow Ti	_			Design F	ows			Se Se	Sewer/Chan	Sewer/Channel Desig	Sewer/Channel Design	Sewer/Channel Design Invertible
1 11		Flow Time To In	Flow Time To In	Flow Time To In	Flow Time Rainfall Unit rate To In Intensity of Runoff Ct	Flow Time Rainfall Unit rate Design Flows To In Intensity of Runoff Cum Flow	Flow Time Rainfall Unit rate Design Flows To In Intensity of Runoff Cum Flow	Flow Time Rainfall Unit rate Design Flows Flow Control	Flow Time Rainfall Unit rate Design Flows Flow Control	Flow Time Rainfall Unit rate Design Flows Flow Ser	Flow Time Rainfall Unit rate Design Flows Flow Sewer/Channel Design To In Intensity of Runoff Cum Flow Control Slope Capacity Velocity	Flow Time Rainfall Unit rate Design Flows Flow Sewer/Channel Design To In Intensity of Runoff Cum Flow Control Slope Capacity Velocity *Dia/

Roof Structure Paved Surface Grass Surface

000

0.95 0.90 0.25

Minimum Velocity = Maximum Velocity =

0.80 m/s 6.00 m/s

Velocity Range:

Time of Concentration:

Time of Concentration =

10 min

Run-off Coefficients Used:

Grass Paved

0.065

Roof

Pipe

4999 Victoria Avenue Niagara Falls, ON L2E 4C9

2 of 2

Exhibit 3 - Pre-Development Wastewater Generation Rate & Peak Drainage Rate 6633 McLeod Road, Niagara Falls

2022-08-16 Job: 220326

WASTEWATER GENERATION ASSESSMENT

			69		
	1600 L/day	Total =			
	1600 L/day	1600 L/dwelling	1 dwelling	1	3 Bedroom Dwelling
Notes	Total Daily Volume	Volume (Table 8.2.1.3, A / B)	Development Statistics	# of Units	Occupancy

Therefore the total calculated sanitary flow from the site is determined to be 1600 L/day.

MAXIMUM PROBABLE DRAINAGE RATE

	10.0 FUs 95.6 L/min	Total = Total Flow =			
	1.5 FUs	1.5 FUs	1 fixture	1	Sink (domestic)
	1.5 FUs	1.5 FUs	1 fixture	_	Clothes washer (private, domestic)
	1 FUs	1 FUs	1 fixture	1	Dishwasher (domestic)
* Existing fixtures were provided by the Owner. Fixtures to be field verified.	6 FUs	6 FUs	1 fixture	1	Bathroom group with flush tank
	Total Sanitary Fixture Units	Fixture Units (Table 7.4.9.3.)	# of Plumbing Fixtures	# of Units	Fixture

Therefore the total calculated peak drainage rate is determined to be 95.6L/min.



Exhibit 4 - Post- Development Wastewater Generation Rate & Peak Drainage Rate 6633 McLeod Road, Niagara Falls

2022-08-16 Job: 220326

WASTEWATER GENERATION ASSESSMENT

	13200 L/day	Total =			
	6600 L/day	275 L/person	4 persons	6	Apartments
	6600 L/day	275 L/person	2 persons	1 12	Apartments
Notes	Volume	8.2.1.3. A / B)	Statistics	# 01 01118	Occupancy
Notac	Total Daily	Volume (Table	Development	# 04 15:45	Occupany

Therefore the total calculated sanitary flow from the site is determined to be 13200 L/day.

MAXIMUM PROBABLE DRAINAGE RATE

		Sink (domestic) 4	Bathroom group with flush tank 4	Dishwasher (domestic) 18	Sink (domestic) 2	Bathroom group with flush tank 2	TXWIE # OF CHIES	
		3 fixtures	4 fixtures	1 fixture	6 fixtures	4 fixtures	Fixtures	, # of Plumbing
Total Flow =	Total =	1.5 FUs	6 FUs	1 FUs	1.5 FUs	6 FUs	(Table 7.4.9.3.)	Fixture Units
325.9 L/min	198.0 FUs	18 FUs	96 FUs	18 FUs	18 FUs	48 FUs	Fixture Units	Total Sanitary
		* Type B Units.	* Type B Units.	* Combined type A and type B units.	* Type A Units.	* Type A Units.		

Therefore the total calculated peak drainage rate is determined to be 325.9L/min.

6633 McLeod Road, Niagara Falls Exhibit 5 - Pre-Development Water Demand

2022-08-16 Job: 220326

DOMESTIC WATER SUPPLY

		Sink (domestic)	Clothes washer (private, domestic)	Dishwasher (domestic)	Bathroom group with flush tank	Fixture	
		_1	1	1	1	# of Units	
		1 fixture	1 fixture	1 fixture	1 fixture	Fixtures	# of Plumbing
Total Flow =	Total =	2 FUs	1.4 FUs	1.4 FUs	3.6 FUs	(Table 7.6.3.2.A.)	Fixture Units
80.3 L/min	8.4 FUS	2	1.4 FUS	1.4 FUS		11	Total Water
					* EX		

s 3.6 FUs * Existing fixtures were provided by the Owner. Fixtures to be field verified.

Therefore the maximum domestic water demand is determined to be 80.3 \perp min.

3 of 5



6633 McLeod Road, Niagara Falls Exhibit 6 - Post- Development Water Demand

2022-08-16 Job: 220326

DOMESTIC WATER SUPPLY

	Sink (domestic)	Bathroom group with flush tank	Dishwasher (domestic)	Sink (domestic)	Bathroom group with flush tank	Fixture
	4	4	18	2	2	# of Units
	3 fixtures	4 fixtures	1 fixture	6 fixtures	4 fixtures	# of Plumbing Fixtures
Total =	2 FUs	3.6 FUs	1.4 FUs	2 FUs	3.6 FUs	(Table 7.6.3.2.A.)
Total = 159.6 FUs Total Flow = 292.7 L/min		57.6 FUs	25.2 FUs	24 FUs	28.8 FUs	Fixture Units
	* Type B Units.	_* Type B Units.	* Combined type A and type B units.	* Type	* Type A Units.	

Therefore the maximum domestic water demand is determined to be 292.7 L/min.



6633 McLeod Road, Niagara Falls **Exhibit 7 - Fire Water Demand**

2022-08-16 Job: 220326

	F	IRE	V	VAT	ER	SI	JΡ	PL	γ
:						_	_	_	=

Building Type:

No Fire Protection

Floor Area

Reduct.

First Floor

333.1 m²

333.1 m²

333.11665 m² 1.00

Second Floor Third Floor

1.00 333.1 m²

333.11665 m² 333.11665 m²

999.34995 m²

Construction Type:

Wood Frame Construction

1.00

Construction Coefficient

1st Preliminary Fire Flow =

10000 L/min

Fire Hazard:

Non-Combustible

Fire Hazard Factor: Net Decrease =

-0.25

-2500 <u>L/min</u>

2nd Preliminary Fire Flow =

7500 L/min

Sprinkler System:

No System

Sprinkler System Factor: No Change =

0.0

0 L/min

Separation Factor

North South 45+ m 0.00 40 m 0.05 8 m

30 m

West East

0.20 0.10 0.35

Net Increase =

2625 L/min

FINAL FIRE FLOW =

10000.0 L/min

Minimum Water Supply Flow Rate for Fire Protection as determined by the Water Supply For Public Fire Protection, dated 1999, by the Fire Underwriter's Survey