NOISE & VIBRATION STUDY

"5687 FERRY STREET DEVELOPMENT" ALL OF LOTS 51, 57 & 58 PART of LOTS 50, 52, 53 & 56 PLAN 3 CITY OF NIAGARA FALLS, ON REGIONAL MUNICIPALITY OF NIAGARA

Prepared for:

RKO Enterprise Inc. 1225 French Road Mount Hope, ON LOR 1W0

Alves

Frank Westaway Owner/President

June 2022 Our File No: 22-2275

dBA Acoustical Consultants Inc. P.O Box 32059 1447 Upper Ottawa Hamilton, ON L8W 3K0

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1.0 INTRODUCTION

dBA Acoustical Consultants Inc. has been asked to provide a noise & vibration study on behalf of RKO Enterprise Inc. for the proposed "5687 Ferry Street Development" in Niagara Falls, ON. (See Attached Figure 1 Site Location).

The purpose of the study is to determine, for OPA/ZBA approval, the traffic noise impact from Ferry Street, Niagara Falls, ON. Proposed is an 8-storey mixed-used apartment building consisting of 77 apartment units and 3 commercial units on the first floor.

This study will detail noise impact relative to the proposed site plan and recommend the noise control measures necessary (if applicable) to meet Ministry of Environment, Conservation and Parks (MECP) guidelines, while satisfying the planning requirements of the City of Niagara Falls and Niagara Region.

Rail noise was not considered in this report as there are no CN/CP rail lines within the immediate area. Aircraft noise was not considered in this report as the development is located outside the 25 NEF of any area airports. Vibration is not considered in this report due to no industry in the area.

2.0 SITE DESCRIPTION

The proposed development is in an area largely comprised of commercial properties and residential properties. Highway 20 (Ferry Street) is located approximately 30m south of building façade. Main Street is located approximately 300m west of the proposed site and Stanley Avenue is located approximately 300m east of the proposed site. Both roadways are not considered main noise sources due to the distance separation and shielding from existing buildings. Ferry Street is a 2-lane roadway with a speed limit of 50km/hr. and runs east and west. Traffic volumes for other area roadways are not considered in this report due to low traffic volumes. There are no area stationary noise sources that may impact the proposed development. See Figure 2 Site Plan.

3.0 NOISE IMPACT ASSESSMENT 3.1 NOISE CRITERIA

The MECP specifies limits for road noise relative to new residential developments. The MECP Publication 300, Stationary & Transportation Sources-Approval & Planning, specifies the criteria, summarized as follows:

TABLE 1 - Road Traffic Sound Levels Limits							
Time Period L _{eq} (dBA)							
07:00 – 23:00 (16 hr.)	55 Outdoor Living Area (OLA)						
23:00 – 07:00 (8 hr.)	50 Plane of Bedroom Window (POW)						

The OLA refers to an outdoor patio, a backyard, a terrace or other area where outdoor passive recreation is expected to occur on the residential property. Noise levels are calculated at the upper storey bedroom window to represent nighttime (23:00 - 07:00) periods.

Where noise levels estimated in the Outdoor Living Area (OLA) and at an upper storey window (POW) are equal to or less than the values listed in Table 1, no noise control measures are required. Where noise levels exceed Table 1 values, the following action is required:

TABL	TABLE 2 – Noise Control Requirements								
Time Period	Noise Level Leq (dBA)	Action Required							
07:00 - 23:00 Daytime (OLA)	55 to 60	Barrier or Warning Clause Type "A"							
07:00 - 23:00 Daytime (OLA)	> 60	Barrier & Warning Clause Type "B"							
07:00 – 23:00 Daytime (POW)	>55	Provision for A/C, Warning Clause "C"							
	>65	Central A/C, Warning Clause "D"							
	>65	Building Component Specification							
23:00 to 07:00 Nighttime (POW)	> 50-60	Provision for A/C and Warning Clause Type "C"							
23:00 to 07:00 Nighttime (POW)	> 60 > 60	Building Component Specification Central Air Conditioning and Warning Clause Type "D"							

Where nighttime noise levels exceed 60 dBA, building components must be designed to meet the following Table 3 indoor sound level limits.

TABLE 3 - Indoor Road Sound Levels Limits							
Leq (dBA)							
Indoor Location	Road						
Living/Dining 7:00 – 23:00	45						
Bedroom 23:00 - 07:00	40						

3.2 ROAD NOISE

Predicted road traffic noise levels were calculated for Ferry Street, the major road noise source in the site area. Road traffic volumes were sourced supplied from the Niagara Region relative to the roadway. MECP computer program STAMSON version 5.04 was used to carry out prediction calculations. For R1 & R2 receptor locations we have confirmed that the traffic noise from Main Street and Stanley Avenue have no noise impact on the proposed site. (See Appendix "A" Attached). Traffic data is summarized in Table 4.

The daytime/night-time volume ratio relative for Ferry Street is calculated using a 90/10 split and a 16/8-hour assessment as required by the MECP. The 2021 AADT (Annual Average Daily Traffic) volumes were forecasted over 21 years and reflective of the worst-case scenario. Truck volumes were factored at 2% medium and 2% heavy of the total vehicle volumes for Ferry Street.

TABLE 4 – Future Road Traffic Volumes (2042)								
Ferry Street	Forecasted AADT 16521 Vehicles							
	Cars	Medium Trucks	Heavy Trucks					
Day	14274	297	297					
Night	14	14						

Table 5 summarizes the "free field" traffic noise prediction results, modeled at 2 receptor location representative of the 2^{nd} & 8^{th} floor south building facade. (See Figure 3 Receptor Locations).

TABLE 5 – Predicted Future Traffic Noise (dBA)								
Location 07:00 - 23:00 23:00 - 07:00								
$R1 - 2^{nd}$ Floor Residential South Façade (7.5m)	60	54						
R2 - 8 th Floor Residential South Façade (28m)	63	56						

4.0 RECOMMENDATIONS - NOISE CONTROL 4.1 OUTDOOR LIVING AREAS

Calculated road noise levels exceed 55 dBA daytime criteria as outlined in Table 1. Proposed for the development are Juliette balconies.

4.2 INDOOR NOISE LEVELS

Calculated road noise levels at the Plane of Window (POW) exceed the 50 dBA criteria outlined in Table 1 for indoor spaces for all receptor locations. Specific building components (walls, windows, doors etc.) are required and confirmed using the STC (Sound Transmission Class) methods and are summarized in Table 6 following with minimum window door and wall construction specified for all residential units throughout the development.

The STC values were calculated for each room type, based on typical window to floor ratios of 20% for bedrooms and 30% for living room areas. Wall-to-floor ratio was factored at 80%. A maximum of two components were factored per room. Windows must meet STC-28 values with acoustical rating. (See Appendix "A")

TABLE 6 – Recommended Door, Wall, and Window Construction									
LOCATIONSTC To Be UsedExterior Wall ConstructionPatio Door Construction									
All Units	Example	Example							
Bedroom	28	40	N/A						
Living room	28	40	N/A						

Recommendations assume windows are well-fitted, weather-stripped units that can be opened.

5.0 VENTILATION / WARNING CLAUSES

Ventilation and Warning Clause requirements are required for this project as noted in Table 7 following. It is recommended that the appropriate warning clauses be inserted into all Offers and Agreements of Purchase and Sale or Lease. Proposed for the development is Central Air Conditioning. It is yet to be determined the location of any HVAC units for this development.

TABLE 7 - Ventilation and Warning Clause Requirements							
LOCATION	WARNING						
		CLAUSE					
All Residential Units	All Residential Units Central Air Conditioning T						

TYPE B:

"Purchasers/tenants are advised that despite the inclusion of noise control features in the development and within the buildings units, sound levels due to increasing road traffic may on occasions interfere with some activities of the dwelling occupants as the sound levels exceed the Municipality's and the MECP's noise criteria."

TYPE D:

"This dwelling unit has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the Municipality's and the MECP noise criteria."

6.0 VIBRATION

Vibration is not a concern as there are no rail or heavy industry located within the site development. The City/Region may require Pre-Condition Survey (PCS) prior to construction and vibration monitoring during construction.

7.0 SUMMARY OF RECOMMENDATIONS

The following noise control measures are required to satisfy the indoor and outdoor noise level criterion:

- Window, door, and wall construction as recommended in Section 4.
- Central Air conditioners for all units.
- Warning Clauses inserted into all Offers and Agreements of Purchase and Sale or Lease for all units. (Section 5.0)
- Supply HVAC units, Generators (Outdoor) and, parking venting system mechanical sound specifications for further noise impact.
- Pre-Condition Surveys and vibration monitoring is recommended due to the close proximity of the abutting properties.
- Qualified Acoustical Consultant certifies that the required noise control measures have been incorporated into the builder's plans prior to issuance of a building permit.
- Qualified Acoustical Consultant certifies that the required noise control measures have been incorporated into the builder's plans prior to issuance of a building permit.
- Prior to issuance of an occupancy permit or equivalent, it is recommended the Qualified Acoustical Consultant certify that the approved noise control measures have been professionally installed.

8.0 CONCLUSIONS

dBA Acoustical Consultants Inc. has provided a noise & vibration study on behalf of RKO Enterprise Inc. for the proposed "5687 Ferry Street Development" in Niagara Falls, ON. (See Attached Figure 1 Site Location).

The purpose of the study determined, for OPA/ZBA approval, the traffic noise impact from Ferry Street, Niagara Falls, ON. Proposed is an 8-storey mixed-used apartment building consisting of 77 apartment units and 3 commercial units on the first floor.

This study detailed noise impact relative to the proposed site plan and recommended the noise control measures necessary to meet MECP guidelines, while satisfying the planning requirements of the City of Niagara Falls and Niagara Region.

FIGURE 1 SITE LOCATION

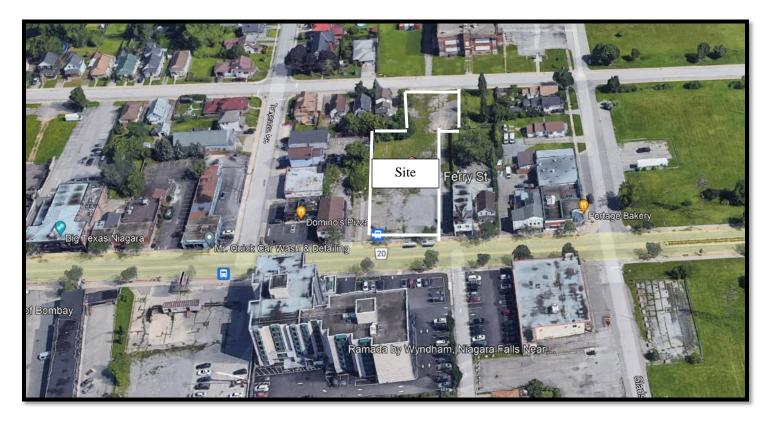
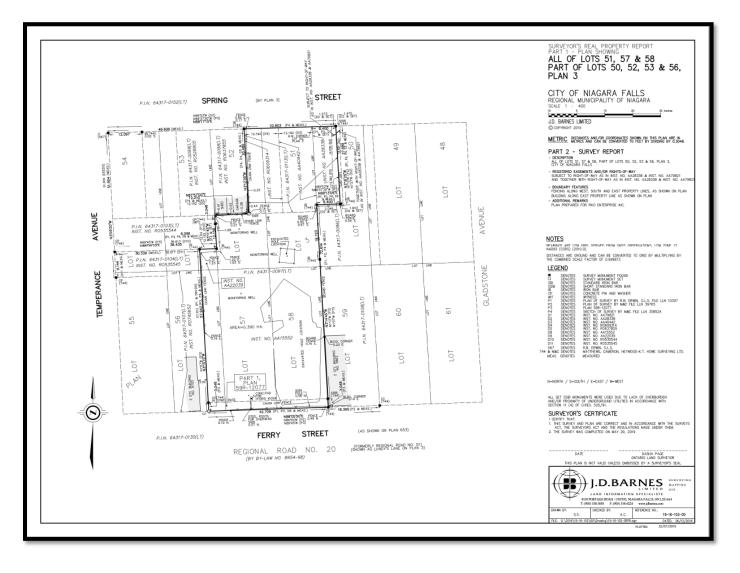


FIGURE 2 SITE PLAN



4.80 15'-9' 3.63 3.00 R2 3.00 30.58 [100'-4"] 3.00 [9'-10'] 3.00 [9'-10'] 3.00 [9-10'] 3.00 9-10'] **R**1 4.15 Ē SOUTH ELEVATION

FIGURE 3 RECEPTOR LOCATIONS

APPENDIX "A"

NIAGARA REGION AADT TRAFFIC DATA (2021)

Hi Frank:

- For Ferry Street between Main and Stanley (RR102) 2021 AADT=10,900; 2018 AADT=12,700
- For Stanley Avenue between Hwy 420 and Ferry Street 2021 AADT=20,600; 2018 AADT=20,500
- For Stanley Avenue between Ferry Street and Robinson Street 2021 AADT=20,000; 2018 AADT=18,900

Regards, Manny Rataul, C.Tech., rcji Road Safety Technician Transportation Services Division, Niagara Region

Phone: 905-980-6000 Ext. 3711 Email: <u>Manny.Rataul@niagararegion.ca</u> Address: 1815 Sir Isaac Brock Way St., Thorold ON, L2V4T7 <u>www.niagararegion.ca</u>

STAMSON CALCULATIONS

SUMMARY REPORT Date: 07-06-2022 12:55:13 STAMSON 5.04 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: R1Ferry.te Time Period: Day/Night 16/8 hours Description: R1 South Front 1st Floor Residential TOTAL Leq FROM ALL SOURCES (DAY): 60.22 (NIGHT): 53.69 Road data, segment # 1: FERRY ST (day/night) _____ _____ Car traffic volume : 14274/1586 veh/TimePeriod * Medium truck volume : 297/33 veh/TimePeriod * Heavy truck volume : 297/33 veh/TimePeriod * Heavy truck volume : 297/33 Posted speed limit : 50 km/h Road gradient : 0 % Road pavement : 1 (Typical asphalt or concrete) * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 10900 Percentage of Annual Growth : 2.00 : 21.00 Number of Years of Growth Medium Truck % of Total Volume : 2.00 Heavy Truck % of Total Volume : 2.00 Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 1: FERRY ST (day/night) _____ Angle1 Angle2 : -90.00 deg 90.00 deg : 0 : 0/0 Wood depth (No woods.) No of house rows Surface : 2 (Reflective ground surface) Receiver source distance : 20.00 / 20.00 m Receiver height : 7.50 / 7.50 m Topography : 1 (Flat (Flat/gentle slope; no barrier) Topography : 0.00 Reference angle Road data, segment # 2: Stanley (day/night) _____ Car traffic volume : 26976/2997 veh/TimePeriod * Medium truck volume : 562/62 veh/TimePeriod * Heavy truck volume : 562/62 veh/TimePeriod * Posted speed limit : 50 km/h Road gradient 0 % : 1 (Typical asphalt or concrete) Road pavement : * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 20600 Percentage of Annual Growth : 2.00 Number of Years of Growth : 21.00 Number of Years of Growth Medium Truck % of Total Volume : 2.00 Heavy Truck % of Total Volume : 2.00 Day (16 hrs) % of Total Volume : 90.00 Data for Segment # 2: Stanley (day/night) _____ Angle1 Angle2 : -45.00 deg 0.00 deg : 0 Wood depth (No woods.) 0 / 0 No of house rows : Surface 1 (Absorptive ground surface) : Receiver source distance : 285.00 / 285.00 m Receiver height : 7.50 / 7.50 m Topography : 1 : 0.00 1 (Flat/gentle slope; no barrier) Reference angle

Result summary (day)						
	2	! !	Road Leq (dBA)	! !	Leq (dBA)	
1.FERRY ST 2.Stanley		!	60.13	!	60.13 43.24	
	Total	+	+		60.22	dBA
Result summary (night	=					
1.FERRY ST 2.Stanley	! source ! height ! (m) ! 1.19 ! 1.19	! ! + !	Road Leq (dBA) 53.60 36.69	! ! !	Leq	
	+	+	+			

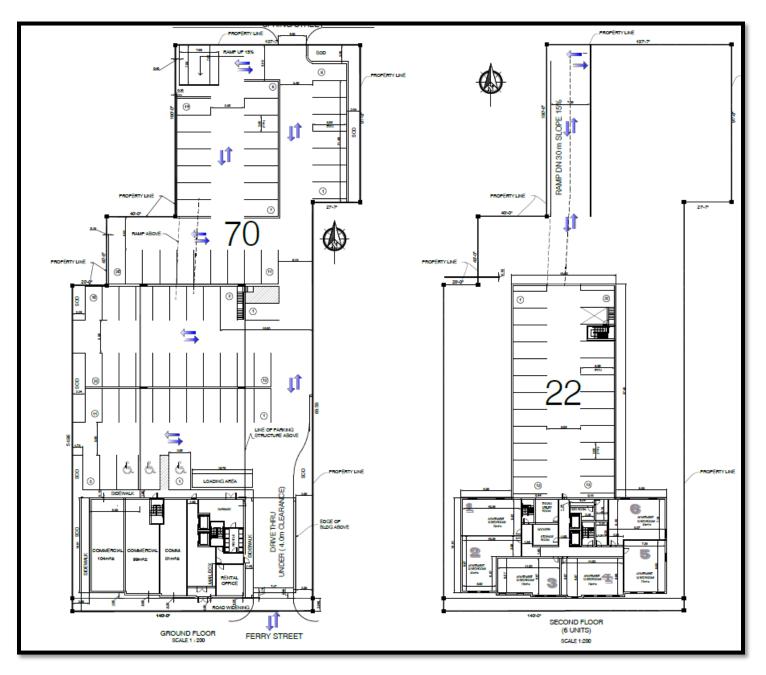
Total

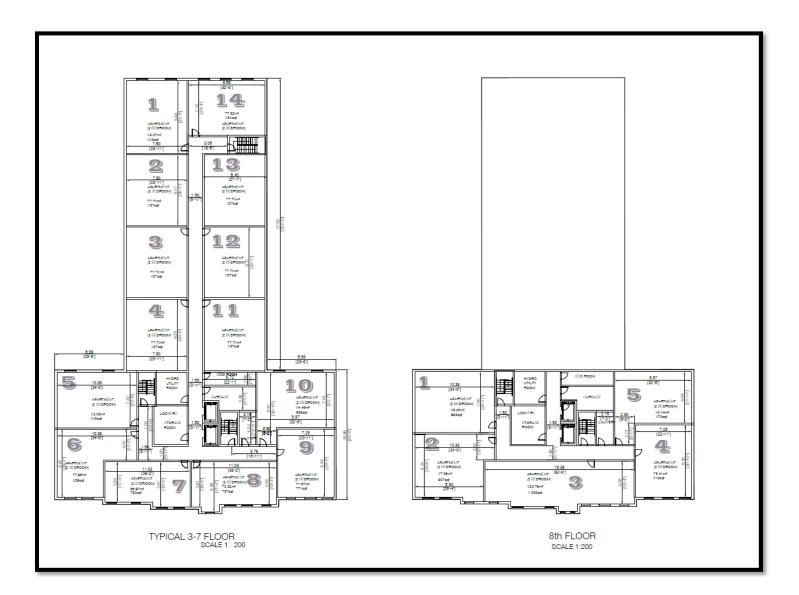
53.69 dBA

Date: 07-06-2022 13:01:25 STAMSON 5.04 SUMMARY REPORT MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Time Period: Day/Night 16/8 hours Filename: r2ferry.te Description: R2 South Front Facade 8th Floor Residential TOTAL Leq FROM ALL SOURCES (DAY): 62.97 (NIGHT): 56.44 Road data, segment # 1: FERRY ST (day/night) Car traffic volume : 14274/1586 veh/TimePeriod * Medium truck volume : 297/33 veh/TimePeriod Heavy truck volume : 297/33 veh/TimePeriod * Posted speed limit : 50 km/h Road gradient : 0 % Road pavement 1 (Typical asphalt or concrete) : * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 10900 Percentage of Annual Growth : 2.00 Number of Years of Growth : 21.00 Medium Truck % of Total Volume : 2.00 Heavy Truck % of Total Volume : 2.00 Day (16 hrs) % of Total Volume : 90.00 Day (16 hrs) % of Total Volume Data for Segment # 1: FERRY ST (day/night) _____ Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods No of house rows : 0 / 0 Surface (No woods.) 0 / 0 (Reflective ground surface) Receiver source distance : 20.00 / 20.00 m Receiver height : 28.00 / 28.00 m : 1 (Flat/gentle slope; no barrier) Topography Reference angle 0.00 : Road data, segment # 2: Stanley (day/night) _____ Car traffic volume : 26976/2997 veh/TimePeriod * Medium truck volume : 562/62 veh/TimePeriod * veh/TimePeriod * Heavy truck volume : 562/62 50 km/h Posted speed limit : Road gradient 0 % : Road pavement : 1 (Typical asphalt or concrete) * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 20600 Percentage of Annual Growth : 2.00 : 21.00 Number of Years of Growth Medium Truck % of Total Volume : 2.00 Heavy Truck % of Total Volume : 2.00 Data for Segment # 2: Stanley (day/night) -----Angle1 Angle2 : -45.00 deg 0.00 deg 0 Wood depth (No woods.) : : No of house rows 0 / 0 1 Surface (Absorptive ground surface) Receiver source distance : 285.00 / 285.00 m Receiver height: 28.00 / 28.00 mTopography: 1 (FlatReference angle: 0.00 1 (Flat/gentle slope; no barrier)

Result summary (day)						
	! source ! height ! (m)	!	Road Leq (dBA)	!	Leq	
1.FERRY ST 2.Stanley	! 1.19 ! 1.19		62.76 49.73		62.76 49.73	
	Total	1	I		62.97	dBA
Result summary (nigh	t) 					
	! source ! height ! (m)		Road Leq (dBA)	!	Total Leq (dBA)	
1.FERRY ST 2.Stanley	! 1.19 ! 1.19		56.23 43.18		56.23 43.18	
	Total				56.44	dBA

BUILDING DESIGNS





SITE STATISTICS

<u>SITE STATISTIC</u>
SITE AREA 3765m ²
BUILDING AREA
GROUND FLOOR 5,091 sqf (473m²) SECOND FLOOR 6,727 sqf (625m²) 3rd-4th FLOORS (PER FLOOR) 14,154 sqf (1,315m²) 5th-7th FLOORS (PER FLOOR) 13,024 sqf (1,210m²) EIGHT FLOOR 5,532 sqf (514m²)
FIRST FLOOR LOBBY & COMMERCIAL 3 COMMERCIAL UNITS 2nd FLOOR 6 UNITS
6 APARTMENTS 3-4th FLOOR 14 APARTMENTS PER FLOOR
28 APT. TOTAL
5-7th FLOOR 13 APARTMENTS PER FLOOR 39 APT. TOTAL
8th FLOOR 4 APARTMENTS UNITS
PROPOSED PARKING SPACES 92
TOTAL No OF APARTMENTS 77 TOTAL No OF COMM. UNITS 3

EXTERIOR WALL STC RATINGS

ſ	Wall	EW1	EW2	EW3	EW4	EW1R	EW2R	EW3R	EW5	EW4R	EW6	EW7	EW8
	Configuration											EW5R	
ſ	STC Rating	38	40	43	46	47	48	49	54	55	57	58	62

Source:

National Research Council, Division of Building Research

NOTES:

- 1 The common structure of walls EW1 to EW5 is composed of 12.7mm gypsum board, vapour barrier and 38x89 mm studs with 50 mm (or thicker) mineral wool or glass fibre batts in interstud cavities.
 - EW1 denotes the common structure, plus sheathing, plus wood siding or metal siding and fibre backer board
 - EW2 denotes the common structure, plus rigid insulation (25 to 30 mm), and wood siding or metal siding and fibre backer board.
 - EW3 denotes simulated mansard with the common structure, plus sheathing, 28 X89 mm framing, sheathing and asphalt roofing material
 - EW4 denotes the common structure, plus sheathing and 20 mm stucco.
 - EW5 denotes the common structure, plus sheathing, 25 mm air space, 100mm brick veneer.
 - EW6 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25 to 50 mm), 100 mm back-up block 100 mm face brick.
 - EW7 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25 to 50 mm), 140mm back-up block, 100 mm face brick.
 - EW8 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25 to 50 mm), 200 mm concrete.
- 2 R signifies the mounting of the interior gypsum board on resilient clips.
- 3 An exterior wall conforming to rainscreen design principles and composed of 12.7 mm gypsum board, 100 mm concrete block, rigid insulation (25 to 50 mm), 25 mm air space, and 100 mm brick veneer has the same STC as EW6.
- 4 An exterior wall described in EW1 with the addition of rigid insulation (25 to 50 mm) between the sheathing and the external finish has the same STC as EW2.